# THE SOLUBILITY OF *n*-ALKANES C<sub>13</sub>H<sub>28</sub> TO C<sub>36</sub>H<sub>74</sub> AND OF SOME BINARIES IN VARIOUS ORGANIC SOLVENTS

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## **Abstract**

The solubility of two *n*-alkanes in commercial organic liquids, such as diesel fuel and jet fuel represent a problem to industry, because they precipitate in an unpredictable fashion. First we calculated the metastable enthalpy and entropy of fusion of the low temperature forms of the *n*-alkanes. We analyzed the solubility of alkanes *n*-C<sub>22</sub>H<sub>46</sub>, *n*-C<sub>23</sub>H<sub>48</sub>, *n*-C<sub>24</sub>H<sub>50</sub> and *n*-C<sub>28</sub>H<sub>58</sub> in ethylbenzene, *m*-xylene, *n*-heptane and gas oil. All systems seem to be close ideal, possibly with a slight positive deviation. We analyzed the solubility at constant temperature of the ternary system solvent C<sub>22</sub>H<sub>46</sub>-C<sub>24</sub>H<sub>50</sub>, C<sub>22</sub>H<sub>48</sub>-C<sub>24</sub>H<sub>50</sub>, C<sub>13</sub>H<sub>28</sub>-C<sub>16</sub>H<sub>34</sub>, C<sub>20</sub>H<sub>42</sub>-C<sub>22</sub>H<sub>46</sub>, C<sub>20</sub>H<sub>42</sub>-C<sub>22</sub>H<sub>46</sub>, C<sub>20</sub>H<sub>42</sub>-C<sub>24</sub>H<sub>50</sub> and C<sub>20</sub>H<sub>42</sub>-C<sub>28</sub>H<sub>58</sub>, and looked at cloud points in various ternary systems. When the difference in the number of carbon atoms in the two alkanes is small, four or less, a metastable solid solution precipitates from the solvent. If the difference in the number of carbon atoms is six or more, the 'equilibrium' phases, or at least phases with low solubility precipitate.

**Keywords:** enthalphy, entropy, metastable, *n*-alkane, phase diagram, solubility

#### Introduction

The solubility of two *n*-alkanes in commercial organic liquids, such as diesel fuel and jet fuel represent a problem to industry. They precipitate as waxes and plug fuel lines. Reddy [1] applied a thermodynamic model to the systems, in which the properties of the two alkanes were 'combined' into one property. Our aim is to find the thermodynamic reason, why this unpredictable precipitation occurs.

First we will obtain the enthalpy and entropy of fusion of the low temperature form of the n-alkanes from the data of Barbillon  $et\ al.$  [2] and Schaerer  $et\ al.$  [3]. The entropy of fusion explains why the solubility of an n-alkane with an odd

1418–2874/98/ \$ 5.00 © 1998 Akadémiai Kiadó, Budapest Akadémiai Kiadó, Budapesi Kluwer Academic Publishers, Dordrecht number of carbon atoms is the same as that of the n-alkane with one carbon atom less. Using the enthalpy of fusion of the low temperature form of the n-alkanes, we can calculate their solubility in various solvents, compare them with the experimental data of Ghogomu *et al.* [4], Provost and Dirand [5], Beiny and Mullin [6], Bronawell and Hollyday [7] and Holder and Winkler [8]. We will use the  $C_p(L-s)$  model for metals and ceramics [9–11], because its results are not different when we use the values of  $C_p(s)$  and  $C_p(s)$  obtained for various alkanes [12].

## Results

We only evaluate other authors experimental data. The origin and purity of the various compounds are given by these authors. We divide all thermodynamic data by R, the gas constant, and the temperature is expressed in kK (kiloKelvin). The units of H, the enthalpy and other energy terms are in kK, and the entropy S and heat capacity  $C_p$  are dimensionless.

## Binary systems

Table 1 shows the enthalpy of fusion and transition of the various alkanes from the data of Barbillon *et al.* [2], Schaerer *et al.* [3], Provost and Dirand [5] and Beiny and Mullin [6] The metastable enthalpy and entropy of fusion of the low temperature form of the *n*-alkanes is obtained by  $H_{\text{fus}}^* = H_{\text{fus}} + H_{\text{trans}}$  and  $S_{\text{fus}}^* = S_{\text{fus}} + S_{\text{trans}}$ .

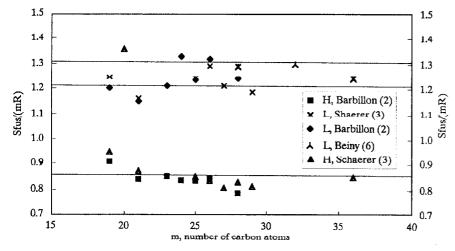
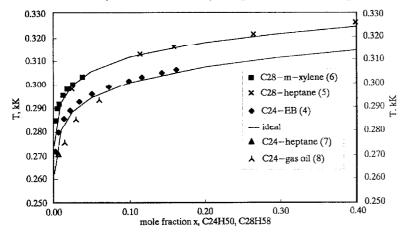


Fig. 1 Entropy of fusion per carbon atom,  $S_{\rm fus}/(mR)$  for n-alkanes, both high H and low L temperature forms. The data of Beiny ( $H_{\rm tus}$  in their paper) gives the value for the low temperature form,  $C_{20}H_{42}$  apparently has only one form, the L form. Value of the horizontal lines:  $S_{\rm fus}/m$  0.856±0.037,  $S_{\rm fus}^*/m$  even 1.308±0.034,  $S_{\rm fus}^*/m$  odd 1.211±0.035

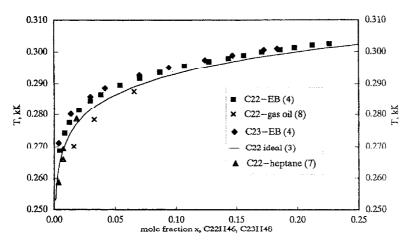
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 $T_{\rm fus}^* = H_{\rm fus}^*/S_{\rm fus}^*$  (the terms marked with \* are the properties of the low temperature forms). We also calculated the entropies of fusion per carbon atom  $S_{\rm fus}/m$ . These data are shown in Fig. 1.  $S_{\rm fus}/m$  for all n-alkanes lie on one horizontal line. The  $S_{\rm fus}^*/m$  data fall on two separate lines, one for the alkanes with an even number, the other for alkanes with odd number of carbon atoms. As the solubility curves are determined by  $S_{\rm fus}^*$  (the stability range of the low temperature form is



Gas oil: molecular weight of 250. EB is Ethylbenzene

Fig. 2 Solubility of n- $C_{24}H_{50}$  and n- $C_{28}C_{58}$  in various solvents. All systems are close to ideal. 'ideal': there is no interaction between the alkane and the solvent. The solubility depends only on the properties of the alkane



Gas oil: Molecular weight 250. EB is ethylbenzene

**Fig. 3** Solubility of n- $C_{22}H_{46}$  and n  $C_{23}C_{48}$  in various solvents. All systems are close to ideal. 'ideal': there is no interaction between the alkane and the solvent. The solubility depends only on the properties of the alkane

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**Table 1** Enthalpy and entropy of fusion of the high and low temperature forms of n-alkanes  $\mathbb{Z}_{19}$  to  $\mathbb{C}_{36}$ 

Reference $\frac{H_{task}}{kK}$ $\frac{T_{task}}{K}$ $\frac{T_{task}}{kK}$ $\frac{H_{task}}{kK}$								ì			
18       301.5         19       5.262       305.1       0.903       1.654       2961       6.916         20       399.6       1.654       2961       6.916         21       5.533       313.4       0.841       1.985       3051       7.517         22       316.9       0.852       2.586       313.5       8.871         23       6.285       320.8       0.837       3.789       321.1       10.284         24       6.495       325.7       0.835       3.187       320.0       10.013         25       6.826       326.7       0.843       4.029       325.6       11.246         27       7.217       329.2       0.843       4.177       330.45       11.551         28       7.374       333.95       0.789       4.177       330.45       11.551         29       1.8       7.383       301.4       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       7.599         21       5.737       313.4       0.872       1.862       305.7       7.599	Reference		$H_{\mathrm{fu}s'}$ kK	T <sub>fus</sub> /	S <sub>fus</sub> /m	H <sub>trans</sub> kK	T <sub>trans</sub> / K	$H_{\mathrm{fu}}^*$ kK	$S_{\mathrm{fu}}^*$ m	$T_{\mathrm{fu}s}^*/$ K	$S^*_{\mathrm{fu}}/m$
19       5.262       305.1       0.903       1.654       2961       6.916         20       339.6       339.6       1.684       2961       6.916         21       5.533       313.4       0.841       1.985       3051       7.517         22       316.9       0.852       2.586       313.5       8.871         24       6.495       323.5       0.837       3.789       321.1       10.284         25       6.826       326.7       0.835       3.187       320.0       10.013         26       7.217       329.2       0.843       4.029       325.6       11.246         27       7.374       333.95       0.789       4.177       330.45       11.551         29       7.383       301.4       305.2       0.950       1.661       296.0       7.172         19       5.51.       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       7.599	Barbillon [2]	18		301.5							
20       339.6         21       5.533       313.4       0.841       1.985       305.1       7.517         22       316.9       316.9       7.517         23       6.285       320.8       0.852       2.586       313.5       8.871         24       6.495       323.5       0.837       3.789       321.1       10.284         25       6.826       326.7       0.843       4.029       321.1       10.013         26       7.217       329.2       0.843       4.029       325.6       11.246         27       7.374       333.95       0.789       4.177       330.45       11.551         29       7.383       301.4       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       7.599         21       5.737       313.4       0.872       1.862       305.7       7.599		19	5.262	305.1	0.903	1.654	296.1	6.916	22.833	302.9	1.202
21       5.533       313.4       0.841       1.985       3051       7.517         22       316.9       316.9       7.517       7.517         23       6.285       320.8       0.837       3.789       321.1       10.284         24       6.495       326.7       0.835       3.187       320.0       10.013         25       6.826       326.7       0.843       4.029       325.6       11.246         27       7.374       333.95       0.789       4.177       330.45       11.551         29       7.383       301.4       7.383       1.661       296.0       7.172         19       5.51:       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       7.599		20		339.6							
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23       6.285       320.8       0.852       2.586       313.5       8.871         24       6.495       323.5       0.837       3.789       321.1       10.284         25       6.826       326.7       0.835       3.187       320.0       10.013         26       7.217       329.2       0.843       4.029       325.6       11.246         27       27       28       4.177       330.45       11.551         29       301.4       305.2       0.950       1.661       296.0       7.172         19       5.51:       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       7.599		22		316.9							
24       6.495       323.5       0.837       3.789       321.1       10.284         25       6.826       326.7       0.835       3.187       320.0       10.013         26       7.217       329.2       0.843       4.029       325.6       11.246         27       8.8       7.374       333.95       0.789       4.177       330.45       11.551         29       8.30       8.30       1.661       296.0       7.172         19       5.51       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       7.599         21       5.737       313.4       0.872       1.862       305.7       7.599		23	6.285	320.8	0.852	2.586	313.5	8.871	27.839	318.6	1.210
25       6.826       326.7       0.835       3.187       320.0       10.013         26       7.217       329.2       0.843       4.029       325.6       11.246         27       28       7.374       333.95       0.789       4.177       330.45       11.551         29       18       7.383       301.4       1.661       296.0       7.172         19       5.51       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       309.4       7.599         21       5.737       313.4       0.872       1.862       305.7       7.599		24	6.495	323.5	0.837	3.789	321.1	10.284	31.877	322.6	1.328
26       7.217       329.2       0.843       4.029       325.6       11.246         27		25	6.826	326.7	0.835	3.187	320.0	10.013	30.854	324.5	1.234
27         28       7.374       333.95       0.789       4.177       330.45       11.551         29       18       7.383       301.4       305.2       0.950       1.661       296.0       7.172         19       5.51:       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4         21       5.737       313.4       0.872       1.862       305.7       7.599		26	7.217	329.2	0.843	4.029	325.6	11.246	34.297	327.9	1.319
28       7.374       333.95       0.789       4.177       330.45       11.551         29       18       7.383       301.4       7.383       7.172         19       5.51:       305.2       0.950       1.661       296.0       7.172         20       8.405       309.8       1.357       309.4       309.4         21       5.737       313.4       0.872       1.862       305.7       7.599		27									
29 18 7.383 301.4 19 5.51: 305.2 0.950 1.661 296.0 7.172 20 8.405 309.8 1.357 313.4 0.872 1.862 305.7 7.599	Provost [5]	28	7.374	333.95	682.0	4.177	330.45	11.551	34.720	332.7	1.240
18     7.383     301.4       19     5.51:     305.2     0.950     1.661     296.0     7.172       20     8.405     309.8     1.357     309.4       21     5.737     313.4     0.872     1.862     305.7     7.599		29									
5.51.       305.2       0.950       1.661       296.0       7.172         8.405       309.8       1.357       309.4         5.737       313.4       0.872       1.862       305.7       7.599	Schaerer [3]	18	7.383	301.4							
8.405 309.8 1.357 309.4 5.737 313.4 0.872 1.862 305.7 7.599		19	5.51	305.2	0.950	1.661	296.0	7.172	23.671	303.0	1.246
5.737 313.4 0.872 1.862 305.7 7.599		20	8.405	309.8	1.357		309.4				
		21	5.737	313.4	0.872	1.862	305.7	7.599	24.402	311.4	1.:62

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Reference	7 T	H <sub>fus</sub> / kK	T <sub>fus</sub> / K	$S_{ m fus}/m$	H <sub>trans</sub> / kK	T <sub>trans</sub> / K	$H_{\mathrm{fu}\zeta}^*$ kK	S <sub>fu</sub> ,/m	$T_{ m fus}^*/$ K	$S_{\mathrm{fus}}^*$ /m
	22	5.888	317.2	0.842	3.392	316.2	9.280	29.295	316.8	1.332
	23	6.492	320.7	0.880	2.617	313.7	9.109	28.591	318.6	1.243
	24	6.603	323.8	0.850	3.764	321.3	10.367	32.113	322.8	1.338
	25	6.945	326.7	0.850	3.135	320.2	10.081	31.055	324.6	1.242
	26	7.157	329.5	0.835	3.875	326.5	11.032	33.593	328.4	1.292
	27	7.247	332.0	608.0	3.483	320.3	10.730	32.707	328.1	1.211
	28	7.776	334.4	0.831	4.263	331.2	12.038	36.128	333.2	1.290
	29	7.952	336.6	0.815	3.573	331.4	11.525	34.41 1	334.9	1.137
	30		338.6			335.2				
	36	10.684	349.1	0.850	4.867	345.3	15.551	44.736	347.9	1.242
Beiny [6]	28	12.028	333.3	1.289						
JH	32	14.193	341.0	1.30]						
	36	15.516	347.7	1.240						
Value of the horizontal lines in Fig. 1:	rizontal lin	cs in Fig. 1:								
/11/		0.856	+0.037							

All values divided by R, the gas constant. The properties marked with a \* are those of the low temperature form

±0.034

1.308

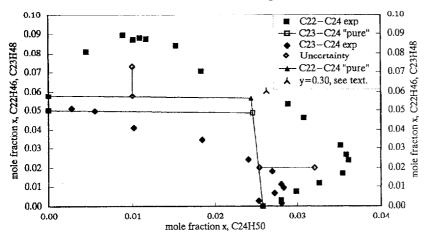
 $S^*_{\text{fus}}/m$  ever  $S^*_{\text{fus}}/m$  odd

much larger) this difference in  $S_{\text{fus}}^*/m$  explains why the solubility of an alkane with odd number of carbon atom falls on the curve of the alkane with one less carbon atoms. The values of the horizontal lines shown in Fig. 1 are also given in Table 1.

Figure 2 shows the solubility of  $n\text{-}C_{24}H_{50}$  and  $n\text{-}C_{28}H_{58}$  in various solvents. The experimentally determined solubility curves fall on the calculated curves, calculated from the data of Barbillon  $et\ al$ . [3] and Provost and Dirand [5]. Similarly Fig. 3 shows the solubility of  $n\text{-}C_{22}H_{46}$  and  $n\text{-}C_{23}H_{48}$  in various solvents. The ideal curve was calculated from the data of Schaerer  $et\ al$ . [3] in Table 1. which as can be seen from Table 1 and Fig. 1 are somewhat different from the data of Barbillon  $et\ al$ . [2]. The data of Bronawell and Hollyday [7] and of Holder and Winkler [8] were read off small graphs. The systems are almost ideal, possibly with small positive deviation. 'ideal' means there is no interaction between the alkane and the solvent: The solubility is independent of the solvent used. The 'ideal' solubility was calculated using our model for metals and ceramics [9–11], as we showed that no difference is found if the heat capacity of the polymers is used [12].

### Ternary systems

Figure 4 shows the solubility of  $C_{22}II_{46}$ – $C_{24}II_{50}$  and  $C_{23}H_{48}$ – $C_{24}H_{50}$  in ethylbenzene at 290 K, calculated from the data of Ghogomu *et al.* [4] in their Table 2.



EB is ethylbenzene. y = 0.30: in the C22-C24 PhD a "metastable miscibility gap" closes.

Fig. 4 Solubility of n-alkane mixtures  $C_{22}$ - $C_{24}$  and  $C_{23}$ - $C_{24}$  in EB at 290 K. Data of Ghogomu et al. [4]. The binary liquid systems are close to ideal. 'ideal': there is no interaction between the alkane and the solvent. The solubility depends only on the properties of the alkane

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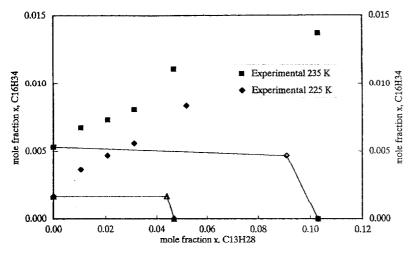
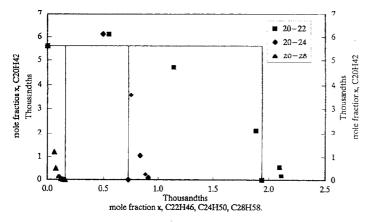


Fig. 5 Solubility of C<sub>13</sub>H<sub>28</sub>-C<sub>16</sub>H<sub>34</sub> *n*-alkane mixtures in Isopar-M at 225 and 235 K. Data of Affens *et al.* [13]. 'pure': pure C2x precipitates. C2x does not interact with the other alkane and the solvent



first vertical line C28, second C24, third C22.

Mol—wt of gas oil 250. Vertical and horizontal lines "pure".

Fig. 6 Solubility of  $C_{20}H_{42}-C_{22}H_{46}$ ,  $C_{20}H_{42}-C_{24}H_{50}$ ,  $C_{20}H_{42}-C_{28}H_{58}$  in gas oil at 290 K. Data of Holder and Winkler [8]. 'pure': pure C2x precipitates. C2x does not interact with the other alkane and the solvent

The 'pure' curves assume that each compound precipitates independently of the other, forming pure solid components: alkane-1 does not interact with alkane-2 or the solvent. The solubility depends only on the properties of alkane-1 resp. alkane-2. The lines deviate somewhat from the horizontal resp. vertical, because when the second component is added, the molfraction of the first component de-

creases. Where the experimental points exceed the 'pure' line, metastable solid phases are precipitating.

In the  $C_{22}H_{46}$ – $C_{24}H_{50}$  system the specially marked point is close to the intersection of the 'pure' curves. The composition of the solid dissolved in the ethylbenzene is y=0.30 (y being the molfraction of  $C_{24}H_{50}$  in the  $C_{22}H_{46}$ – $C_{24}H_{50}$  binary). This is the composition where in an earlier paper [12] we discussed the possibility of a metastable miscibility gap between  $\beta_1'$  and  $\beta_2'$  at 305 K in the  $C_{22}H_{46}$ – $C_{24}H_{50}$  binary system.

The  $C_{23}H_{48}$ – $C_{24}H_{50}$  phase diagram does not show such a pronounced stability of the intermediate phases as the  $C_{22}H_{46}$ – $C_{24}H_{50}$  phase diagram, and no metastable miscibility gap can be drawn. This system precipitates below the pure values, and only close to  $C_{24}H_{50}$  is there possibly a metastable precipitation.

Figure 5 shows the solubility of  $C_{13}H_{28}$ – $C_{16}H_{34}$  in Isopar-M at 225 and 235 K. The data were calculated from Table 4 of Affens *et al.* [13]. We see the same effects as in Fig. 6.

Figure 6 shows the solubility of  $C_{20}H_{42}$ – $C_{22}H_{48}$ ,  $C_{20}H_{42}$ – $C_{24}H_{50}$ , and  $C_{20}H_{42}$ – $C_{28}H_{58}$  in a gas oil at 290 K. The data were calculated from all the points in the small Figs 1, 2 and 3 of Holder and Winkler [8]. The results for  $C_{20}H_{42}$ – $C_{22}H_{48}$  and  $C_{20}H_{42}$ – $C_{24}H_{50}$  are similar to those in Figs 4 and 5. For the  $C_{20}H_{42}$ – $C_{28}H_{58}$  binary the solubility curve drops very rapidly, indicating that no metastable phase or phases are precipitating.

The metastability is probably caused by the fact, that the compounds are stabilized by a large positive entropy, the enthalpy of formation being also positive. The precipitation mechanism and crystal growth process must be further investigated.

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